

Comparison of
Zotter's and Henry and Napoly's formalisms
in deriving a general expression
for longitudinal and Transverse
Resistive Wall impedance

LCU meeting June 18, 2007

E. Métral and B. Salvant

Agenda

- Context
- Henry and Napoly approach (1991)
- Zotter approach
- Comparison for a round infinite layer

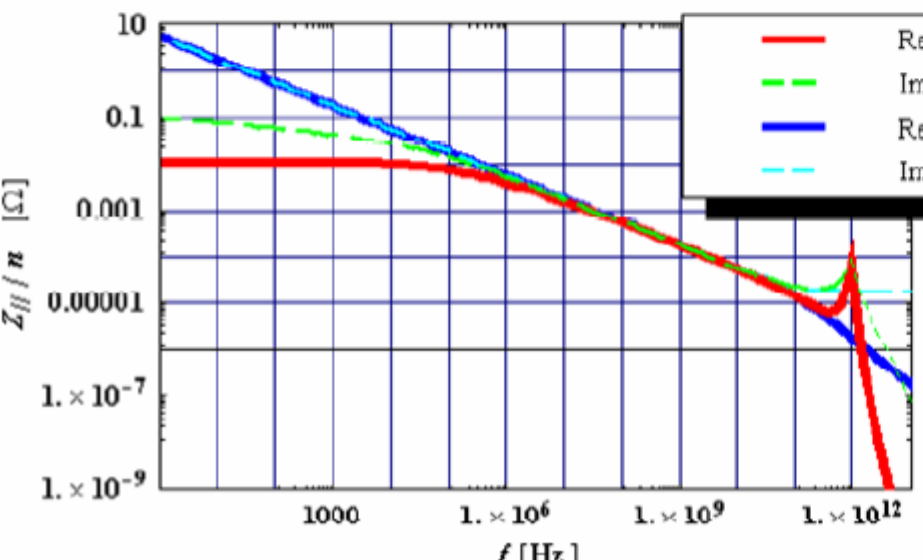
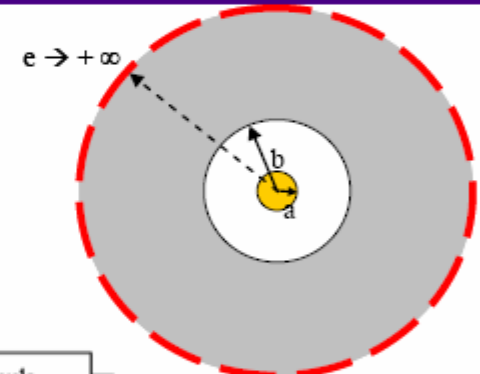
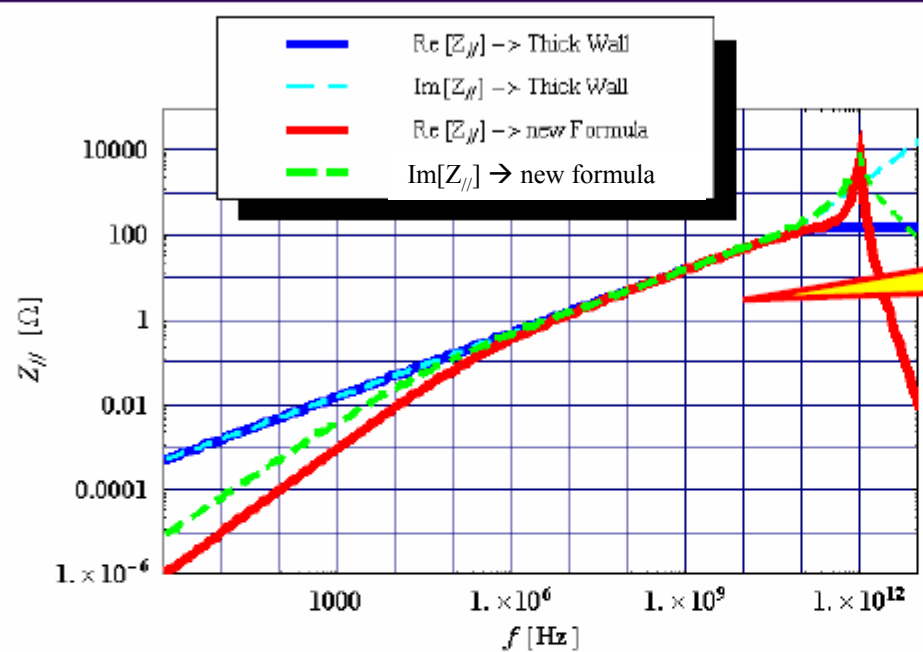
LHC IMPEDANCE STATUS AND STRATEGY

E. Métral with Hubert Medina and Benoit Salvant

- ◆ **The LHC impedance is dominated by the collimators**
- ◆ **Current work**
 - Link the Mathematica program rewall to ZBASE \Rightarrow Hubert Medina
 - General program for the resistive-wall impedance (upgrade of rewall) \Rightarrow Benoit Salvant
- ◆ **LHC collimators Phase II \Rightarrow Video conference on LHC collimation (07/03/07)**
- ◆ **Studies on TCT, TCLI, TCDQ, TCDS and TDI**
- ◆ **More details for the injection and dump septum**
- ◆ **Next important work**
- ◆ **Stability diagram at top energy before the squeeze**
- ◆ **Conclusion**

GENERAL PROGRAM FOR RESISTIVE-WALL IMPEDANCE (2/4)

3 regimes found (as for the transverse)



- beam
- vacuum
- graphite

with
 $b = 2 \text{ mm}$
 Graphite Relaxation Time = $0.8 \cdot 10^{-12} \text{ s}$
 Graphite DC conductivity = $10^5 \text{ S}\cdot\text{m}^{-1}$
 Collimator Length = 1 m

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Henry and Napoly approach (CLIC Note 142 – 1991)

- Longitudinal Impedance Z_z / L

$$Z_z(r, \theta, \omega) = \sum_{m=0}^{\infty} \cos(m\theta) r^m Z_z^{(m)}(\omega)$$

where

$$Z_z^{(m)}(\omega) = -\frac{i\omega Z_0}{\pi c} \left(\frac{r_0}{a^2}\right)^m (m+1) H_m(Ka) \left[\left(m(m+1) - \frac{\omega^2 a^2}{c^2} \right) H_m(Ka) + 2(m+1) \frac{\omega^2 a}{Kc^2} H_{m+1}(Ka) + \frac{\alpha_m}{2} Ka (H_{m+1}(Ka) - H_{m-1}(Ka)) \right]^{-1}$$

with the following notations

$$K = (\pm 1 + i) \sqrt{\frac{|\omega| Z_0 \sigma}{2c}} \quad \text{for } \pm \omega \geq 0$$

and

$$\alpha_m = \begin{cases} 2 & \text{for } m = 0 \\ m + 1 & \text{for } m \geq 1 \end{cases}$$

Mode m



Henry and Napoly approach (CLIC Note 142 – 1991)

- Transverse Impedance Z_{\perp} obtained through the Panofsky-Wenzel Theorem

$$Z_{\perp}(\omega) = \sum_{m=1}^{\infty} m r^{m-1} (\cos(m\theta) \mathbf{e}_r - \sin(m\theta) \mathbf{e}_{\theta}) \frac{ic}{\omega} Z_z^{(m)}(\omega)$$

- **Warning: conventions are different from Henry and Napoly's to Zotter's formalisms:**
 - Henry and Napoly chose not to divide the transverse impedance by i in their definition
 - Henry and Napoly did not normalize the transverse impedance with the offset r_0 of the beam to the center of the pipe
 - Henry and Napoly used the $\exp(-i\omega t)$ convention while Zotter uses the $\exp(j\omega t)$ convention
- Therefore, we have the following relations:

$$Z_{//}^{(Zotter)} = \text{Re}[Z_z^{(0)}] - j\text{Im}[Z_z^{(0)}]$$

$$Z_{\perp}^{(Zotter)} = \frac{1}{r_0} \left(\text{Im}[Z_{\perp}^{(1)}] + j\text{Re}[Z_{\perp}^{(1)}] \right)$$

Henry and Napoly approximation for intermediate and high frequencies (CLIC Note 142 – 1991)

- Approximated longitudinal impedance $Z_{//}$

$$Z_z^{(m)}(\omega) = \frac{1-i}{\alpha_m \pi a} \sqrt{\frac{Z_0 \omega}{2\sigma c}} \left(\frac{r_0}{a^2}\right)^m (m+1) \left[1 - \frac{1+i}{\sqrt{2}\alpha_m} \left(\frac{\omega s_0}{c}\right)^{\frac{3}{2}}\right]^{-1}$$

Approximation valid if:

- the skin depth is much lower than the beam pipe radius $\delta \ll a$
- only the first modes m are considered

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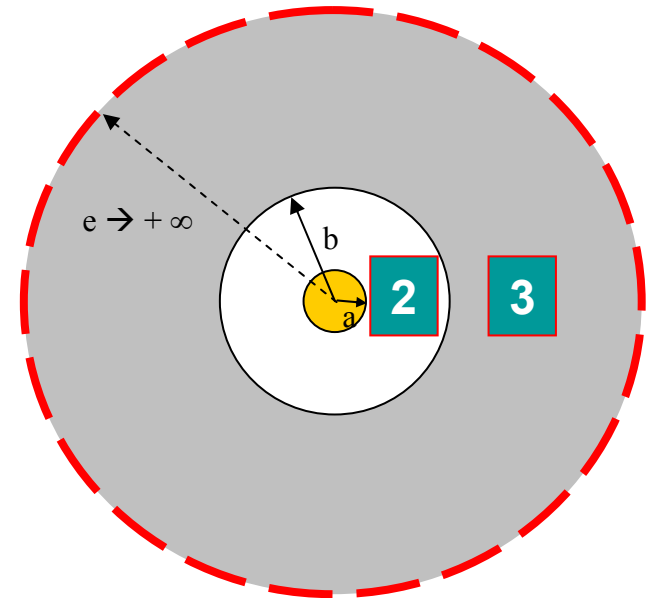
Resistive Wall longitudinal Impedance of... ... a **monolayer** extending to $+\infty$

- Solution:

$$Z_{//}^{RW}(\omega) = -\frac{j\omega L(1-\beta^2\mu_r\epsilon_r)I_0(s)^2}{2\pi\epsilon v^2} \left(\frac{K_0(x)}{I_0(x)} - \alpha_2 \right)$$

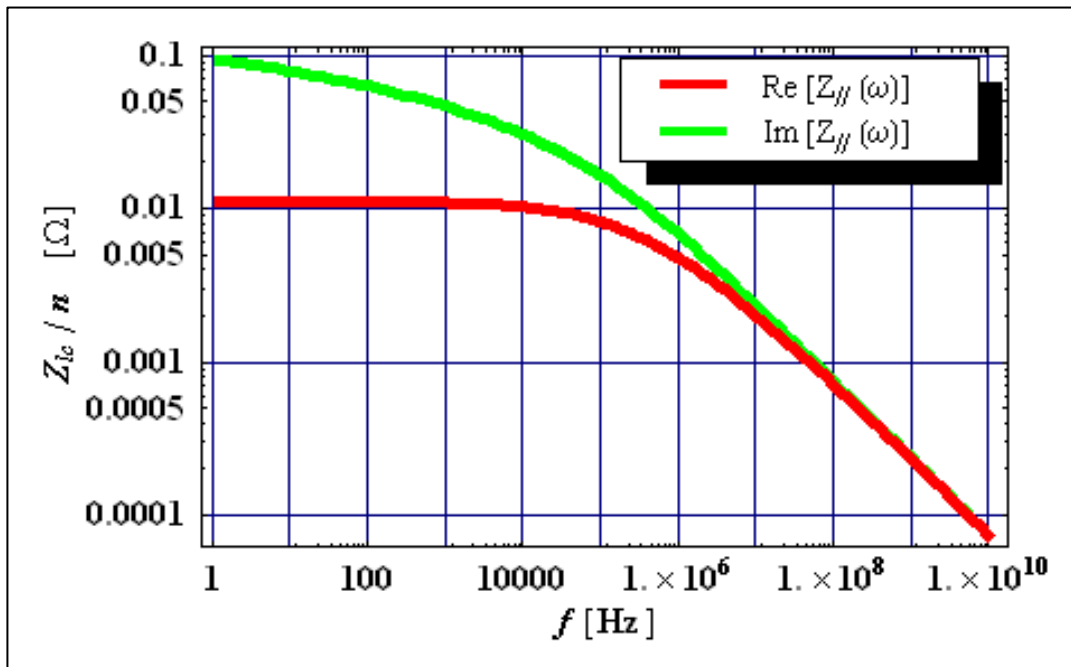
with

$$\alpha_2 = \frac{-\epsilon'_2\nu_3 K_0(\nu_3 b) K_1(\nu_2 b) + \epsilon'_3\nu_2 K_0(\nu_2 b) K_1(\nu_3 b)}{\epsilon'_2\nu_3 I_1(\nu_2 b) K_0(\nu_3 b) + \epsilon'_3\nu_2 I_0(\nu_2 b) K_1(\nu_3 b)}$$



- beam
- vacuum
- graphite

with $b = 1.5$ mm

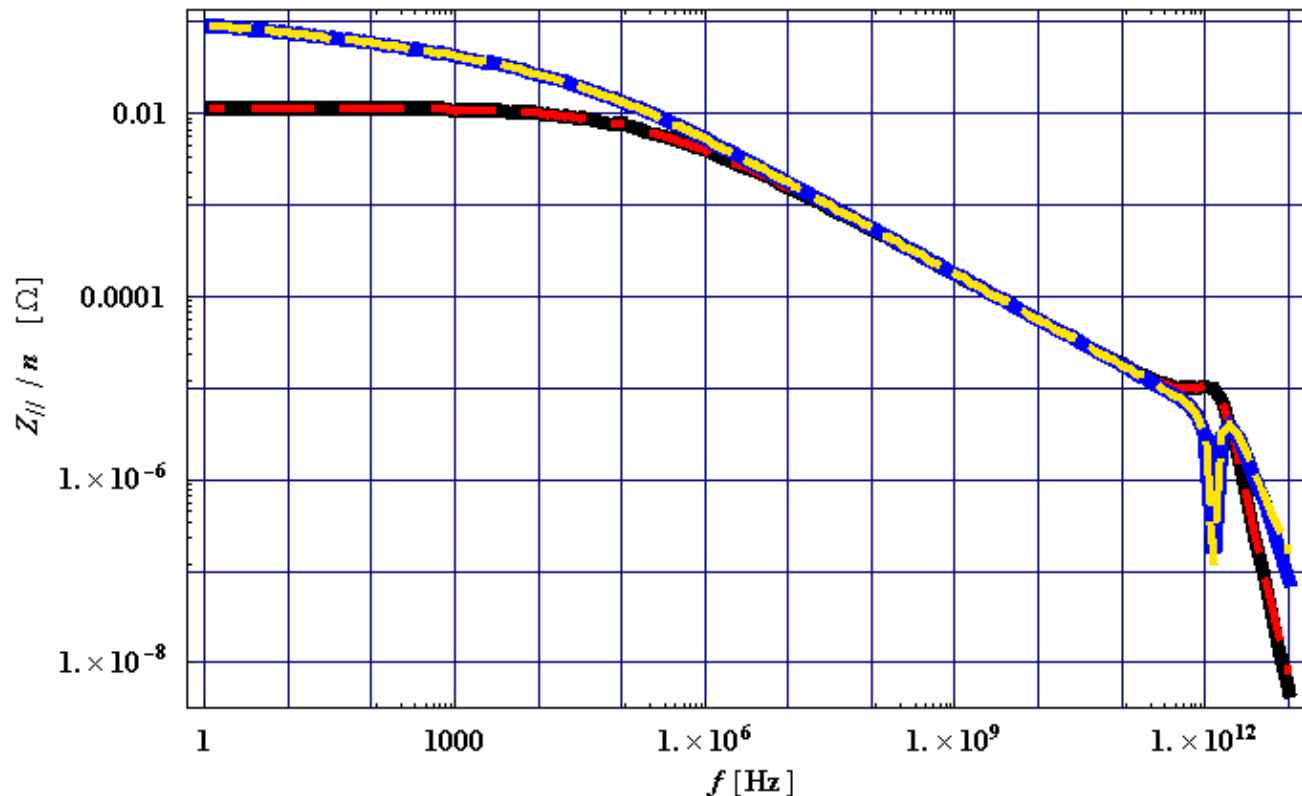
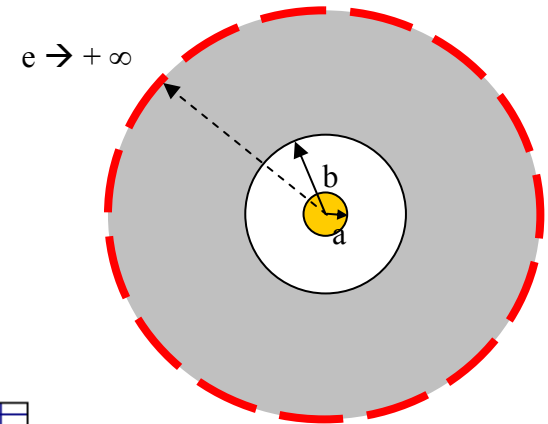
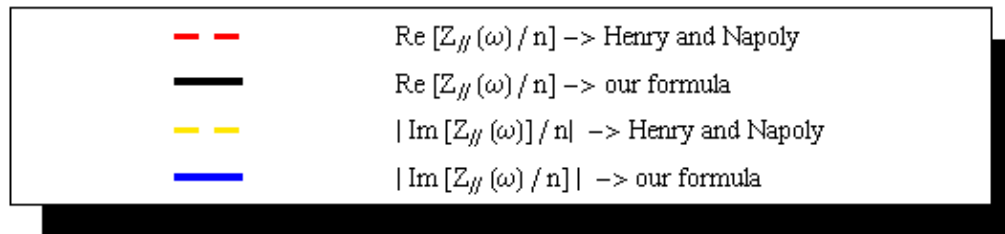





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Henry and Napoly approach compared to Zotter approach

- longitudinal impedance $Z_{||} \rightarrow$ mode 0



-  beam
-  vacuum
-  graphite

with $b = 2$ mm

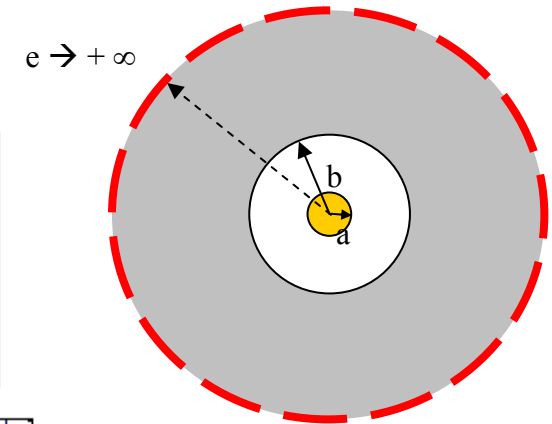
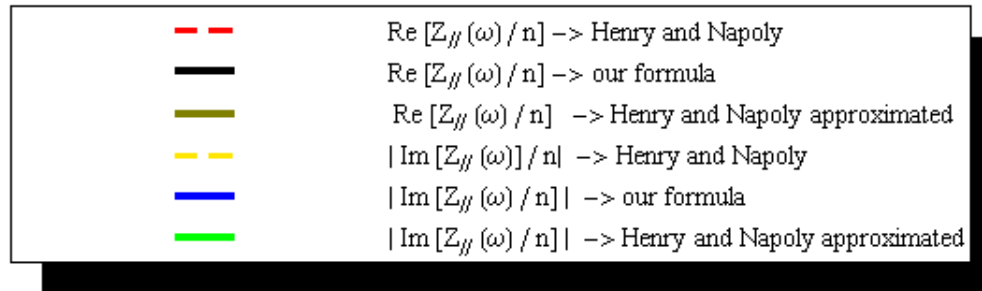
Remarks:




- Perfect agreement until 1THz
- After 1 THz, H&N formula leads CPU precision to its limits.
- H&N formula seems a bit off after 1 THz

\rightarrow to be investigated

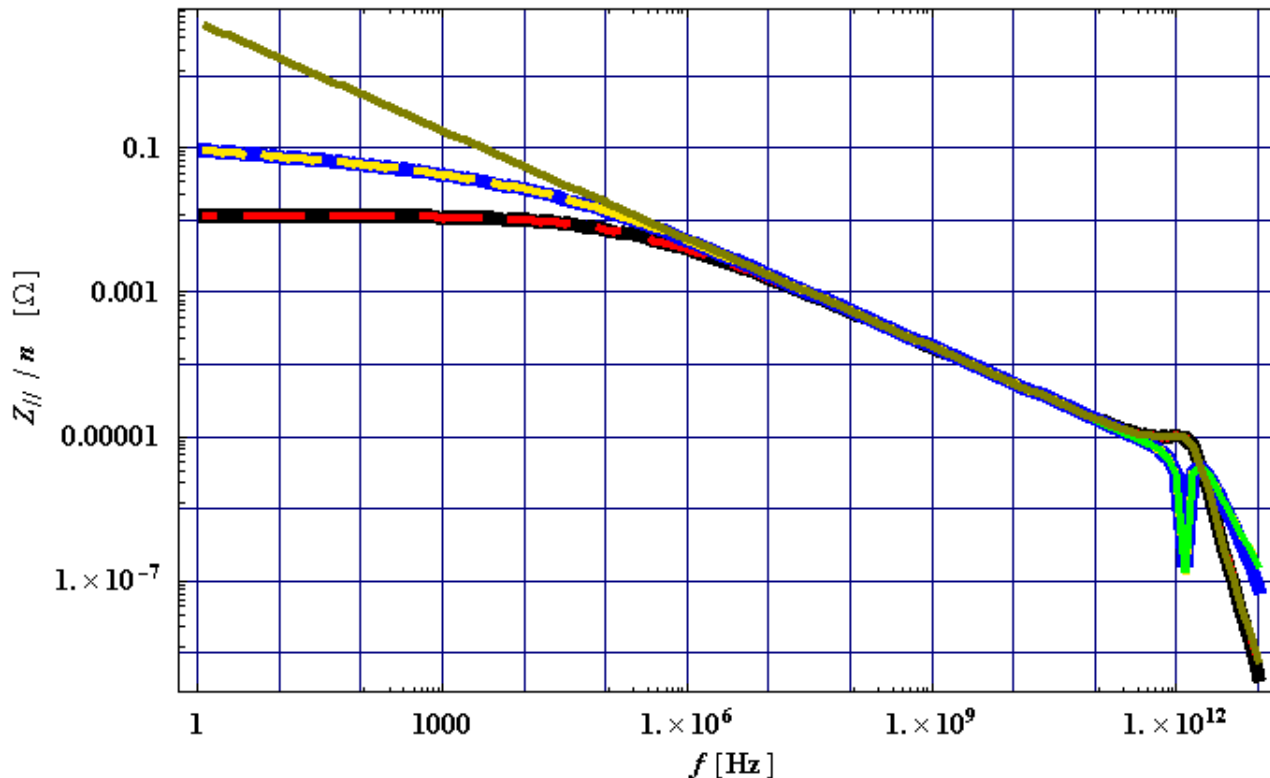
Henry and Napoly approach compared to Zotter approach

- Longitudinal impedance $Z_{||}$ \rightarrow mode 0



-  beam
-  vacuum
-  graphite

with $b = 2$ mm



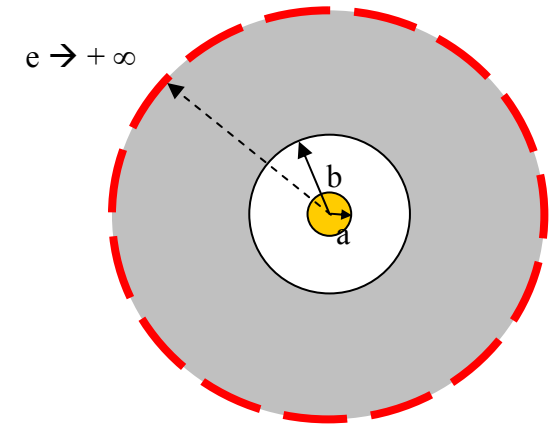
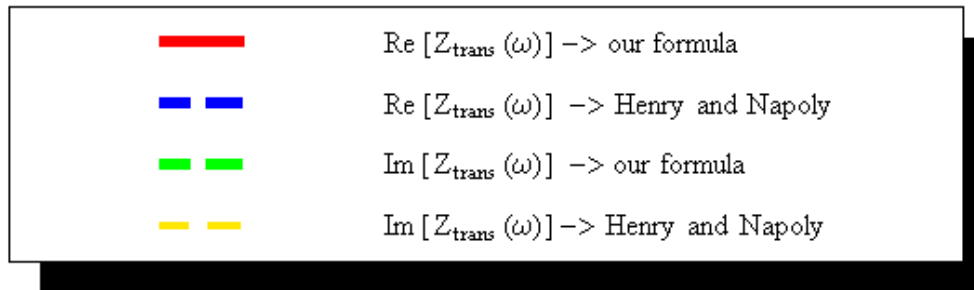
Remarks:




- Perfect agreement until 1THz
- After 1 THz, H&N formula leads CPU precision to its limits.
- Both H&N and Approximated H&N formula seems a bit off after 1 THz

\rightarrow to be investigated

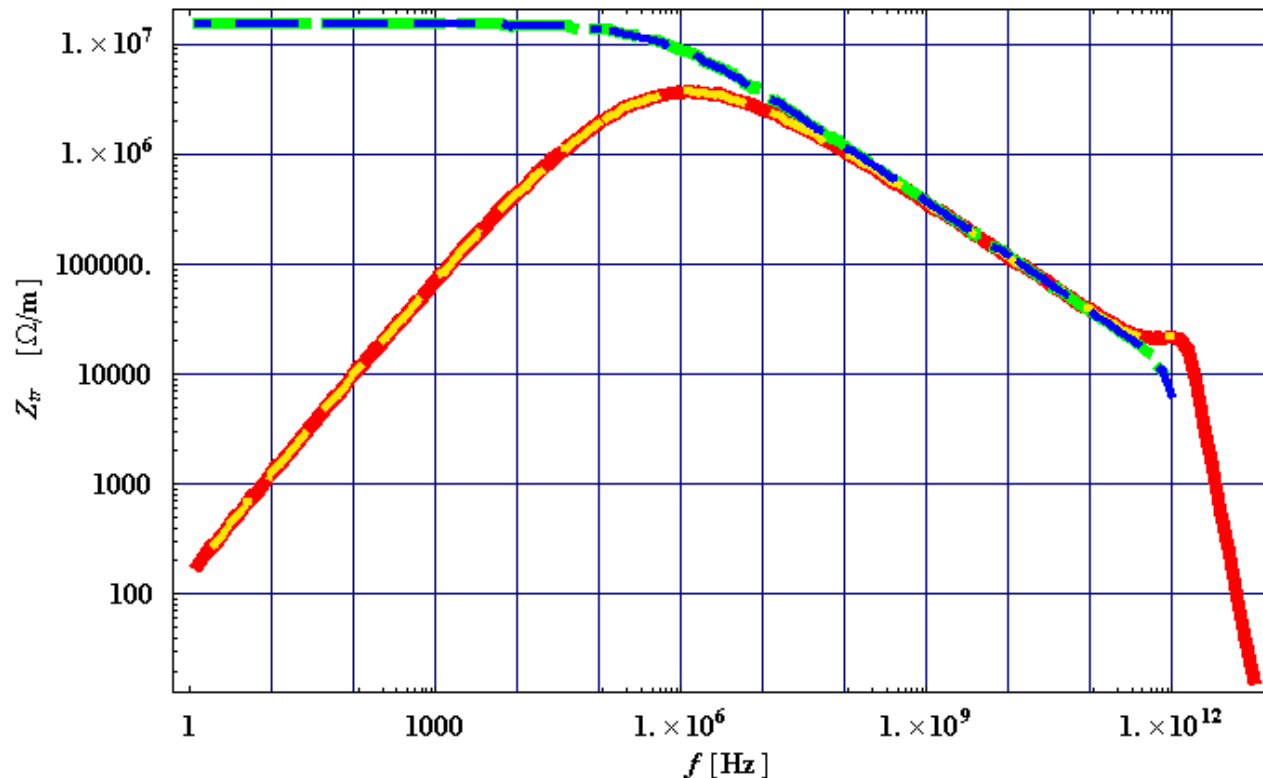
Henry and Napoly approach compared to Zotter approach

- Transverse impedance $Z_{\perp} \rightarrow$ mode 1



 beam
 vacuum
 graphite

with $b = 2$ mm



Remarks:

- Perfect agreement until 1THz
- After 1 THz, H&N formula leads CPU precision to its limits.

Henry and Napoly approach compared to Zotter approach

- **Advantages of Henry and Napoly approach :**
 - All modes can be calculated
 - ➔ enable to use the Panofsky-Wenzel theorem to compute the transverse impedance
- **Advantages of Zotter approach :**
 - Includes non-ultrarelativistic particles
 - Includes Materials with any σ , ϵ_r and/or μ_r
 - Includes Multi-Layer beam pipe
 - Does not lead to CPU precision issues at high frequencies

All our thanks to:

Stéphane Fartoukh